

18 ΦΟΙΤΗΤΙΚΟ ΣΥΝΕΔΡΙΟ
ΕΠΙΣΚΕΥΕΣ ΚΑΤΑΣΚΕΥΩΝ 2012
14-15 ΦΕΒΡΟΥΑΡΙΟΥ 2012

Δυναμική Ευστάθεια Αρθρωτών Κατασκευών

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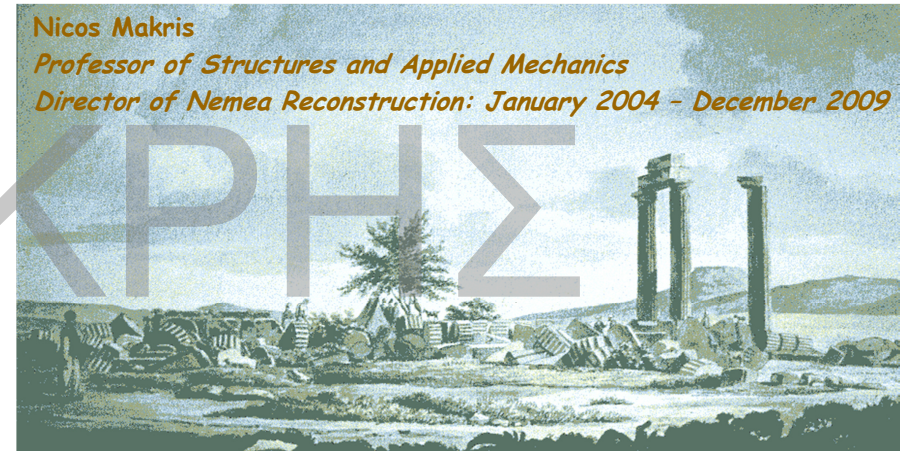
Τομέας Κατασκευών, Πανεπιστήμιο Πατρών

The Reconstruction of the North-East Corner of the Temple of Zeus at Nemea

Nicos Makris

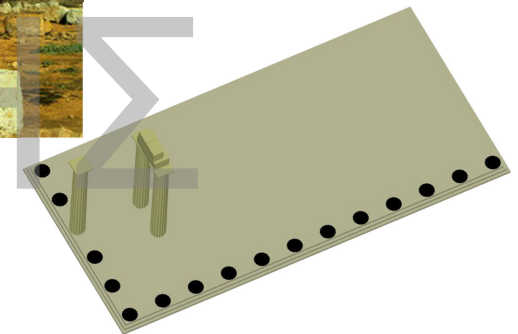
Professor of Structures and Applied Mechanics

Director of Nemea Reconstruction: January 2004 – December 2009



Nemea - Temple of Zeus, 1766

View of the three columns standing from the ancient times



The challenge of reconstruction. Why reconstructing ? Aerial View of the Temple (1977)



Columns have fallen to the outside

5

Erroded column drums



6

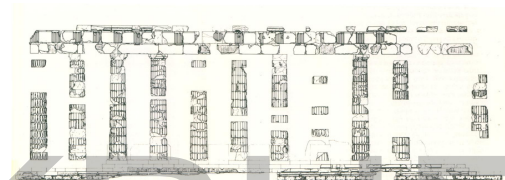
View from the west of the 3 standing columns from ancient times



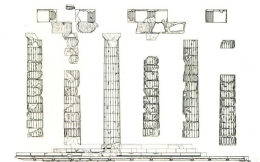
7

Synthesis of the ancient stone blocks by Frederic Cooper (1980-1982), University of Minnesota

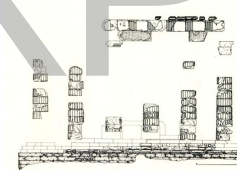
North view



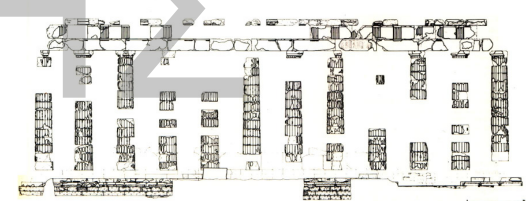
East view



West view

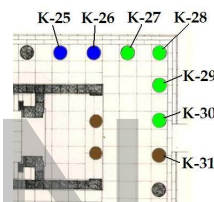
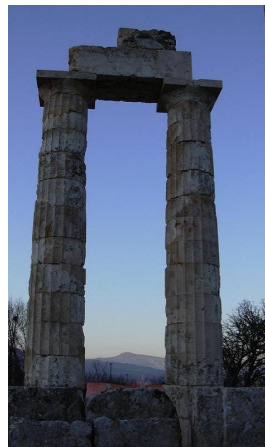


South view



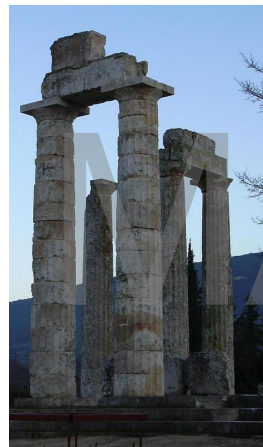
8

Pilot Reconstruction: columns K-25 & K-26



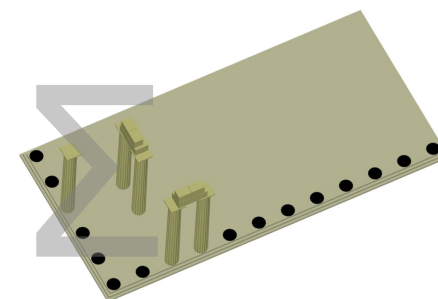
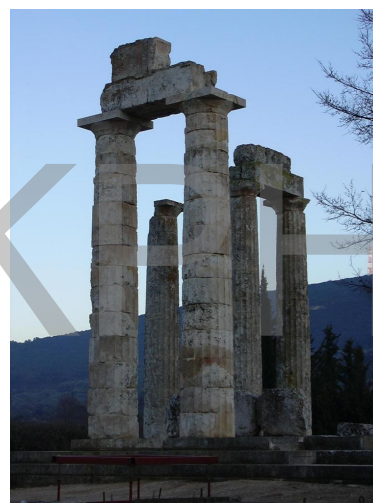
With the invaluable contribution of:

Dr. Kostas Zambas
Prof. Manolis Korres
Mr. Ioannis Arbilias



9

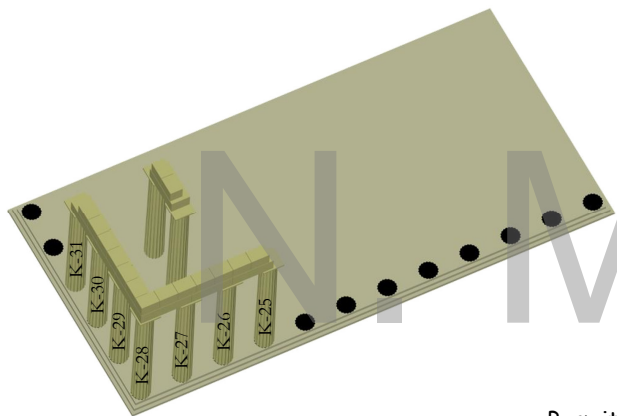
The pilot reconstruction: K-25 & K-26



Completed: Summer 2002

10

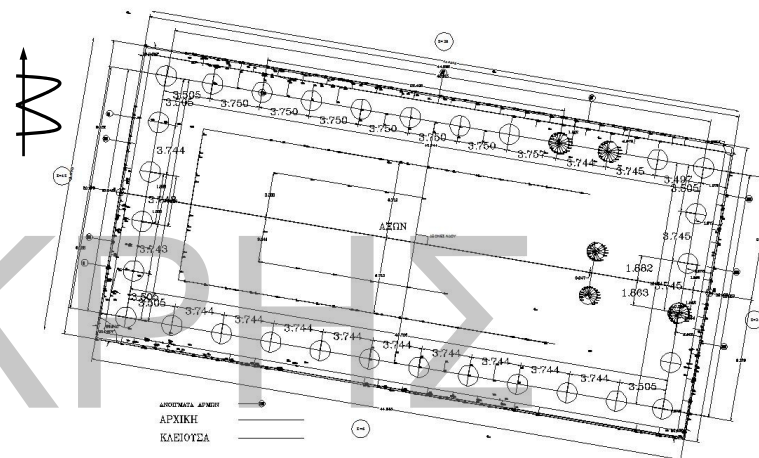
The shape of the temple after the completion of the second phase.
Reconstruction of K-27, K-28, K-29 & K-30



Permit issued on
March 04 2004

11

Detailed surveying of the current situation of the monument



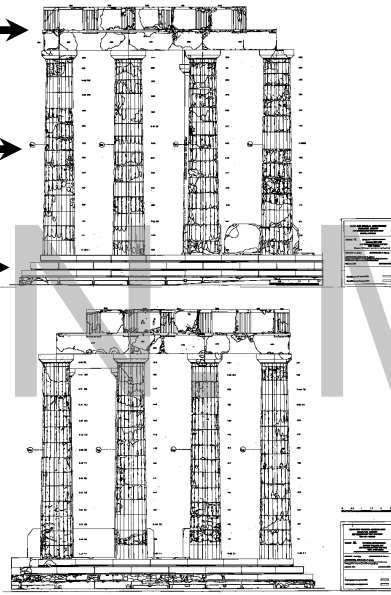
Establishment of the centers of the columns based on a sophisticated optimization analysis

12

Epistyles and Frieze

Columns

Crepida



13

Reconstruction of the crepida



14

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View of retrofitted ancient stones



15

16

Wire-sawing and preparation of new material



17

Retrofit of Δ-25: stylobate of ancient column K-31



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24

Need for retrofitting the column drums



26

View of final result of retrofitted drums



27

Works on existing and new column drums



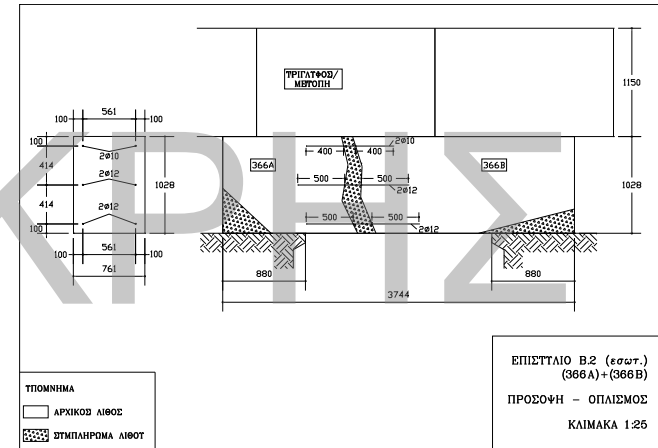
28

View of fragmented epistyles



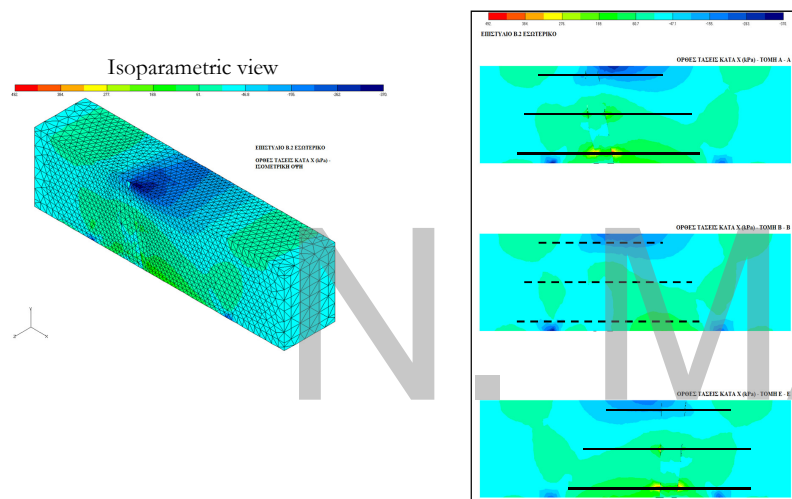
29

Schematic of retrofitted epistyle



30

Normal stresses in the epistyle



31

Les grands oeuvres de l' homme

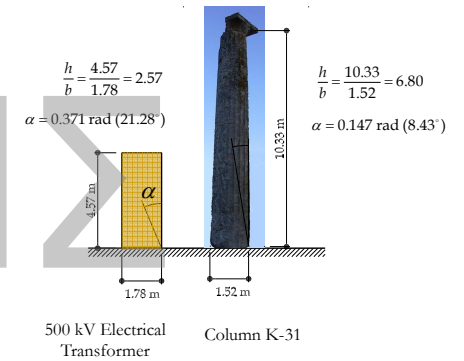


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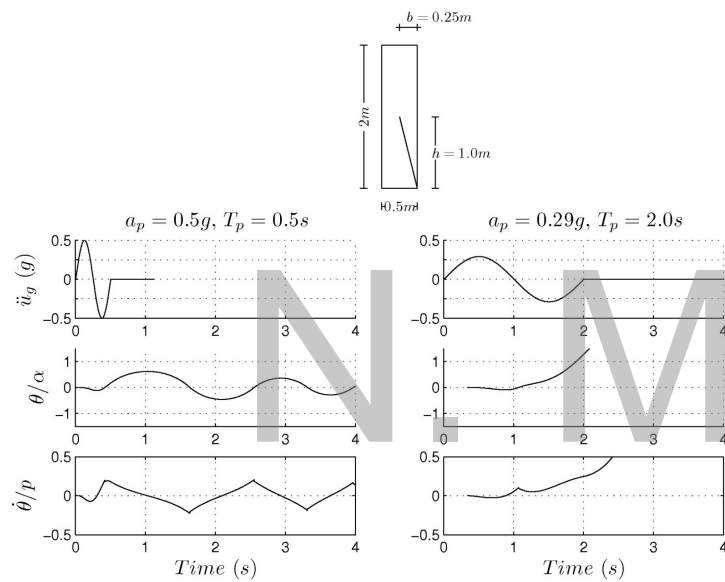


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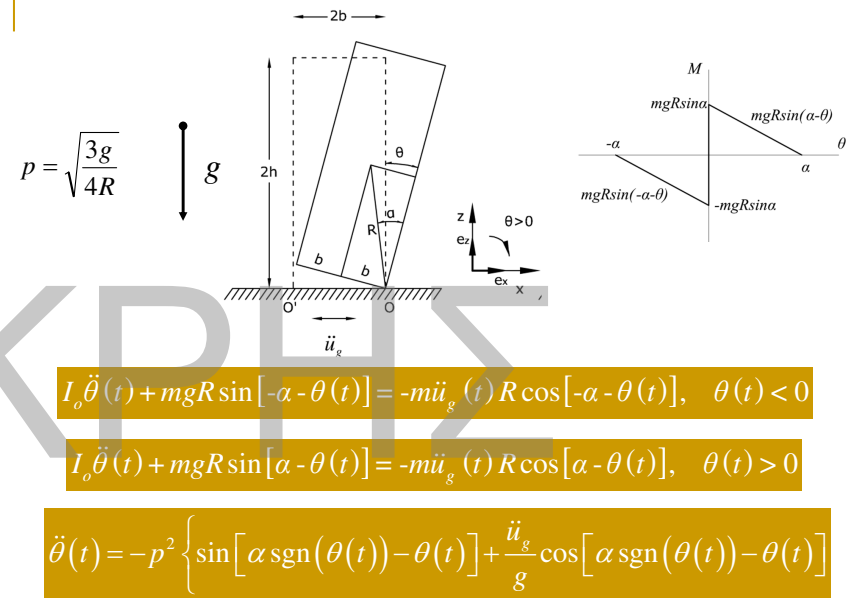
Seismic Stability of free-standing slender structures



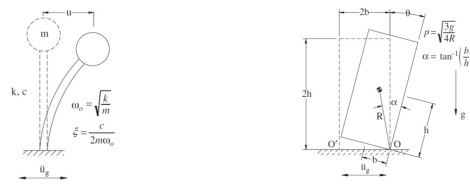
34



35



36



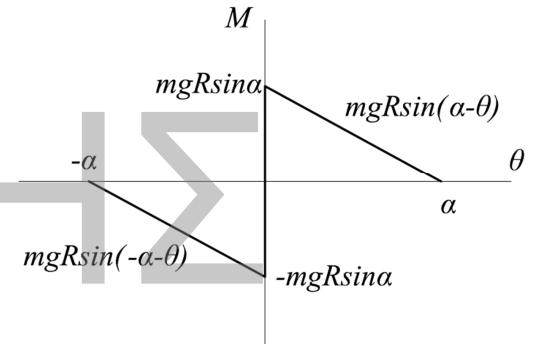
Parameters/ characteristics	Damped oscillator m, c, k	Rocking rigid block b, h, g
Restoring mechanism	Elasticity of the structure	Gravity
Restoring force/moment	$F = ku$ (for linear springs)	$M = mgR \sin(\alpha - \theta)$ $R = \sqrt{b^2 + h^2}$
Stiffness at stable equilibrium	Finite	Infinite
Restoring force/moment at stable equilibrium	Zero	Finite: $mgR \sin(\alpha)$
Stiffness away from equilibrium	Positive	Negative
Frequency parameter	Undamped natural frequency: $\omega_0 = \frac{2\pi}{T_0} = \sqrt{\frac{k}{m}}$	Frequency parameter: $p = \sqrt{\frac{3g}{4R}}$ (for rectangular blocks)
Damping parameter	Viscous damping ratio: $\xi = \frac{c}{2m\omega_0}$	Slenderness: $\alpha = \tan^{-1}(b/h)$

37

$$I_0 \dot{\theta}_1 - m \dot{\theta}_1 2bR \sin(\alpha) = I_0 \dot{\theta}_2$$

$$r = \frac{\dot{\theta}_2^2}{\dot{\theta}_1^2}$$

$$r = \left[1 - \frac{3}{2} \sin^2 \alpha\right]^2$$



38

Dimensionless Products

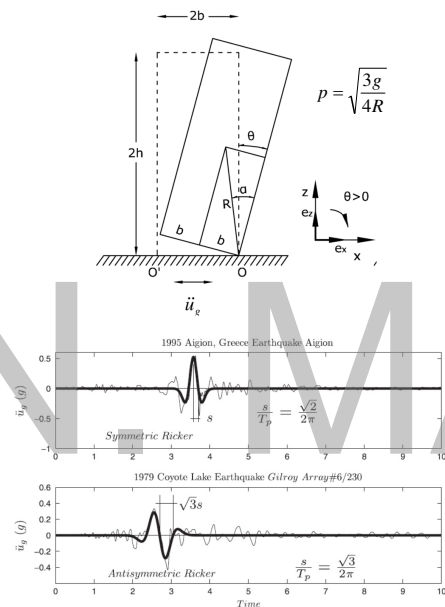
$$\Pi_\theta = \theta$$

$$\Pi_\omega = \frac{\omega_p}{p}$$

$$\Pi_\alpha = \tan(\alpha)$$

$$\Pi_g = \frac{a_p}{g}$$

$$\theta(t) = \varphi\left(\frac{\omega_p}{p}, \tan \alpha, \frac{a_p}{g}\right)$$

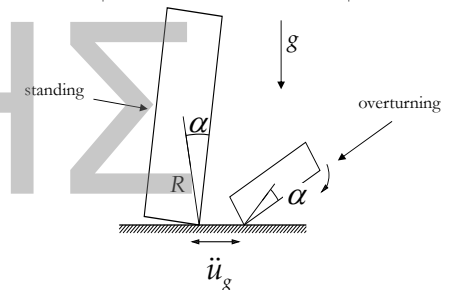


39

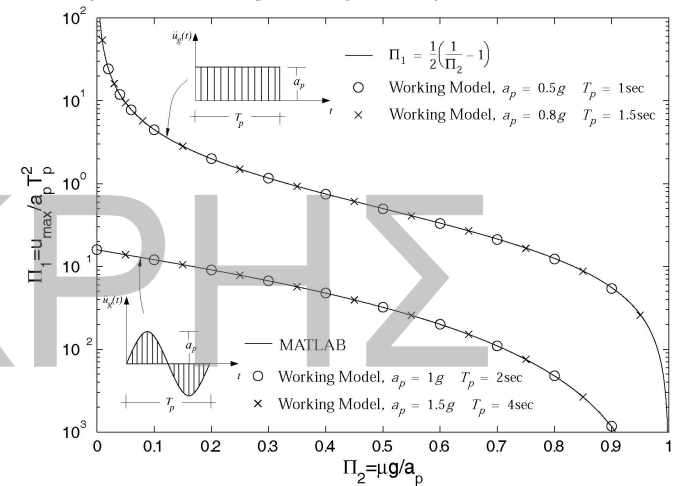
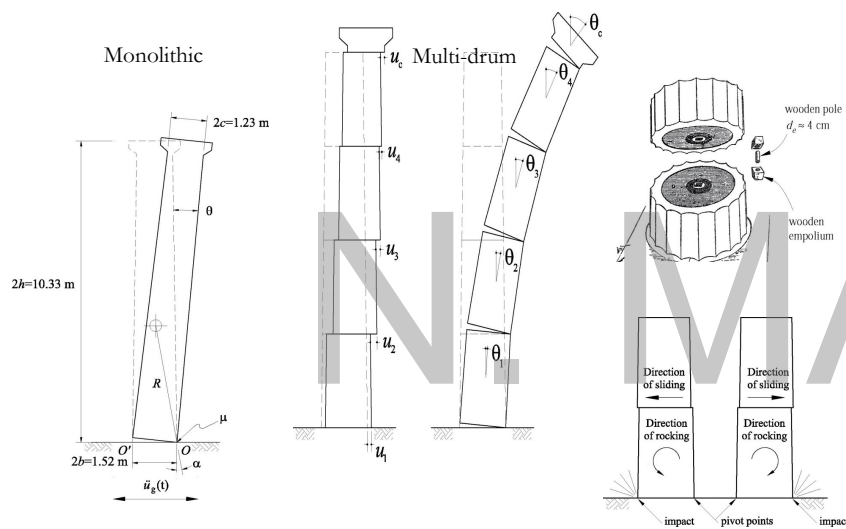
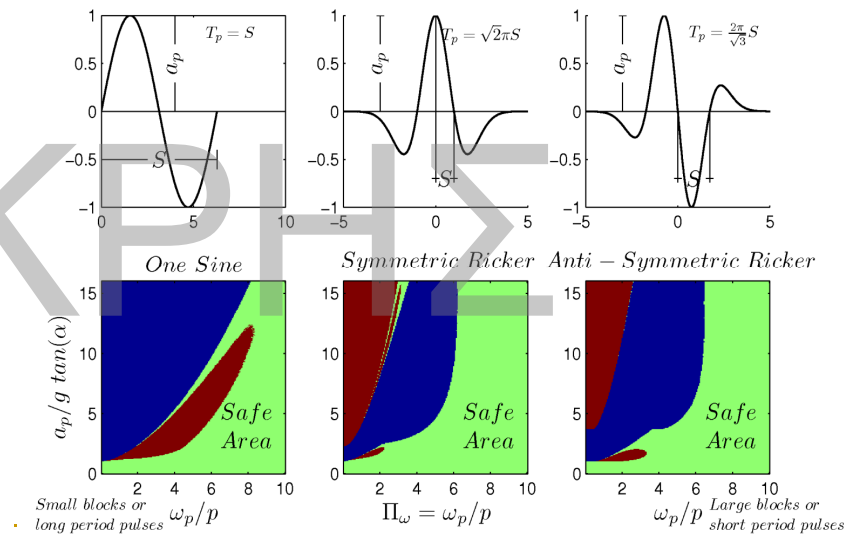
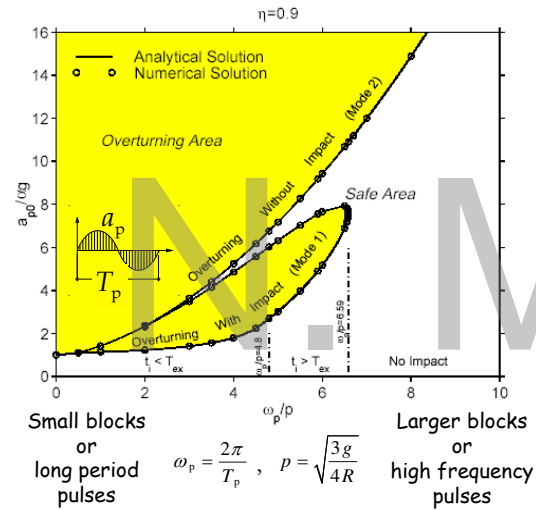
Fundamental size-frequency effect: 1963 George W. Housner

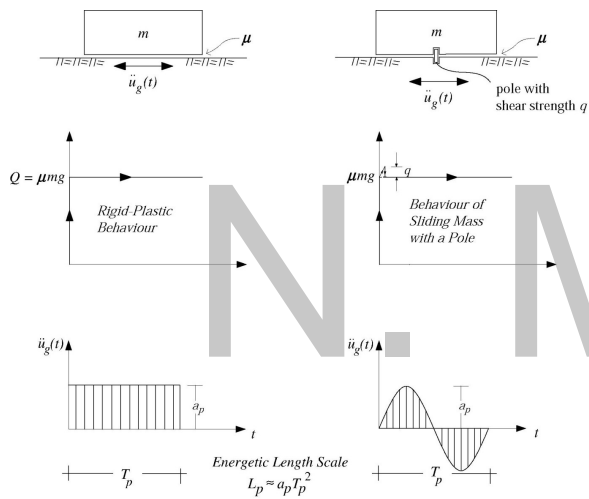
(a) The larger of two geometrically similar blocks can survive the excitation that will topple the smaller block; and (b) out of two same acceleration-amplitude pulses the one with the longer duration is more capable to induce overturning

Conclusion reached from studies motivated from the destruction observed after the May 1960 earthquake in Chile.

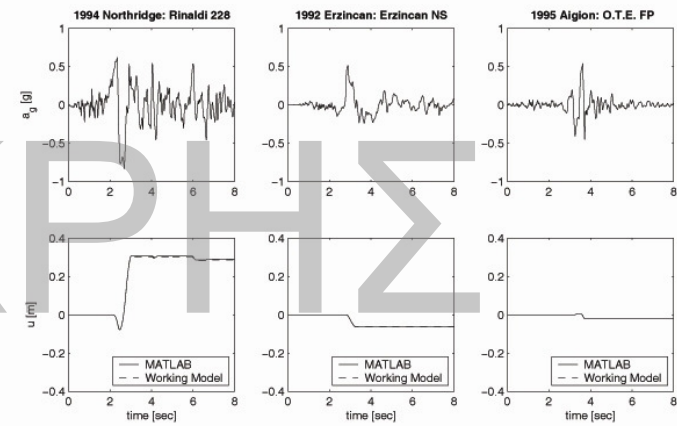


40

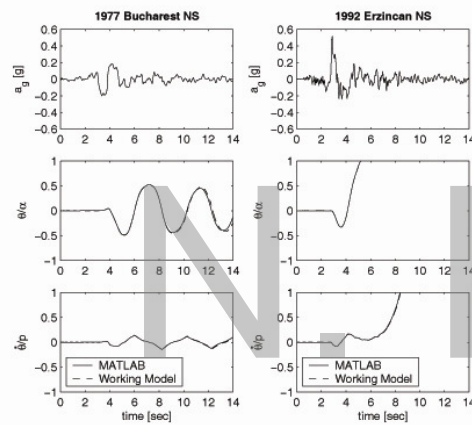




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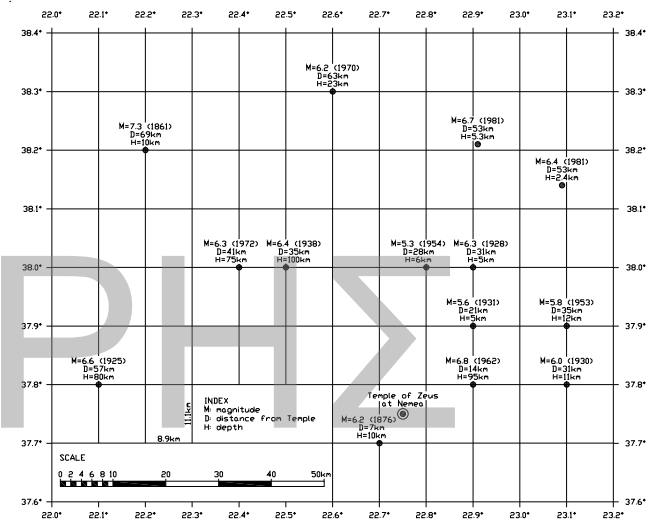


46



47

Seismic Hazard



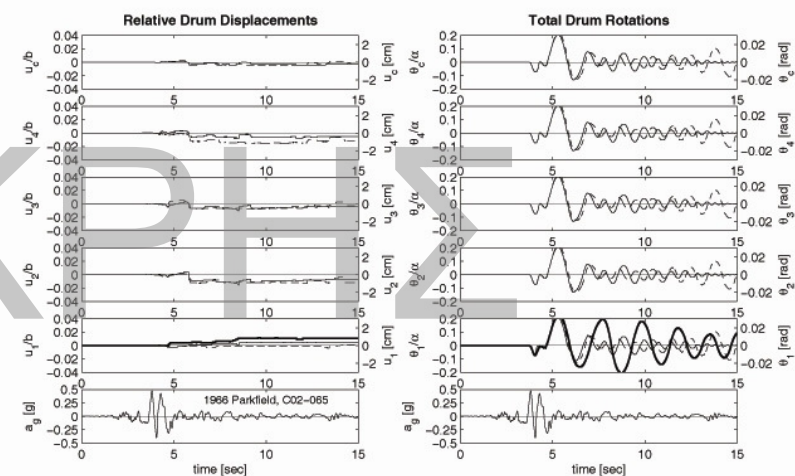
Location of selected historic earthquakes nearby the Temple of Zeus at Nemea.

48

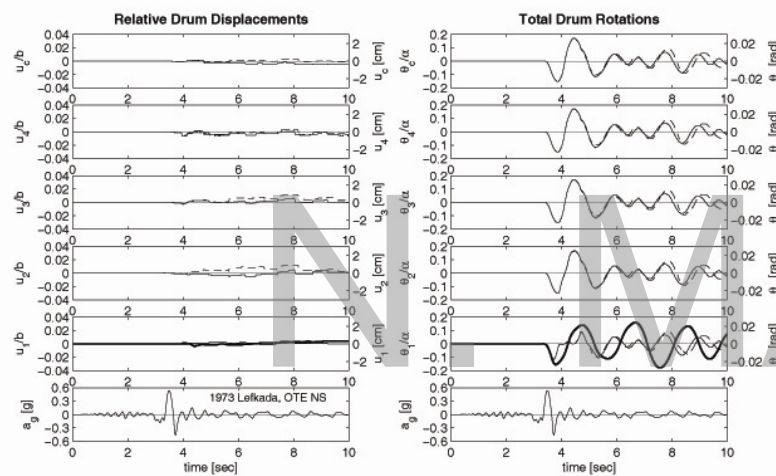
Table. Seismic Records that Represent to the Extent Possible the Seismic Hazard of the Area of the Temple of Zeus.

EARTHQUAKE	DATE	MAGN. M	RECORDING STATION	LOCAL SITE CONDITIONS	DIST. D (km)	PGA g	PGV cm/sec	PGD cm
Superstition Hills	1987 Nov. 24	6.7	El Centro Imperial Country	soil	13.9	0.36	46.4	16.0
			Westmoreland Fire Station	soil	13.3	0.21	31.0	20.1
Northridge	1994 Jan. 17	6.7	Simi Valley, Katherine Rd	soil	14.6	0.88	40.8	5.3
			Sun Valley, Roscoe Blvd	soil	12.3	0.44	38.3	10.0
Parkfield	1966 June 28	6.1	Temblor	rock	9.9	0.36	21.4	3.5
Leukada	1973 Nov. 04	6.0	OTE building	soil	20	0.53	55.0	11.6
Aigion	1995 June 15	6.2	OTE building	soft rock	18	0.50	43.3	7.1
Kalamata	1986 Sept. 13	6.0	Nomarthia building	hard soil	5.0	0.27	24.2	5.6
Parnitha	1999 Sept. 07	5.9	Sepolia B	13 m deposits of limestone	8.0	0.32	21.5	2.7
Bucharest	1977 March 04	7.2	Bucharest	soil	160	0.20	73.4	20.4
Kocaeli	1999 Aug. 17	7.4	Sakarya	soil	3.1	0.38	79.4	71.4

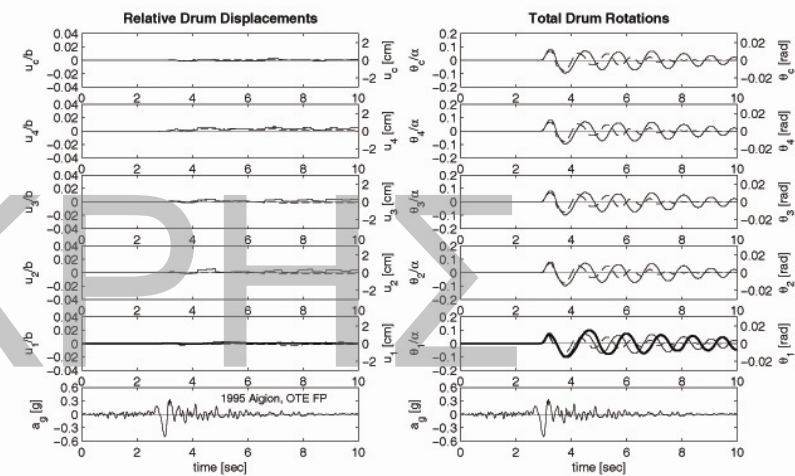
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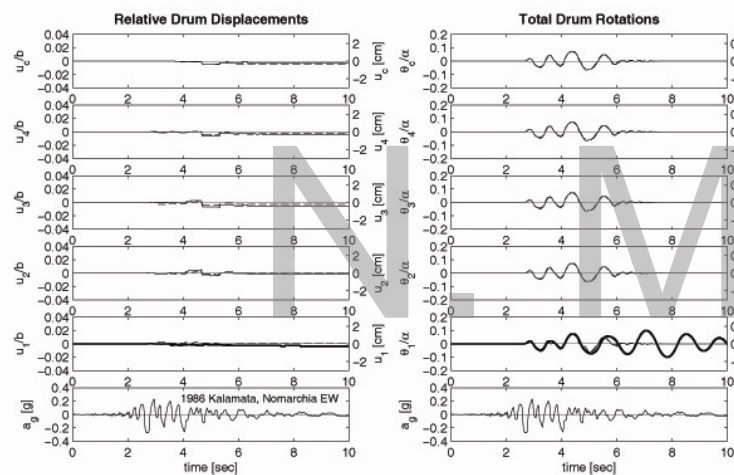
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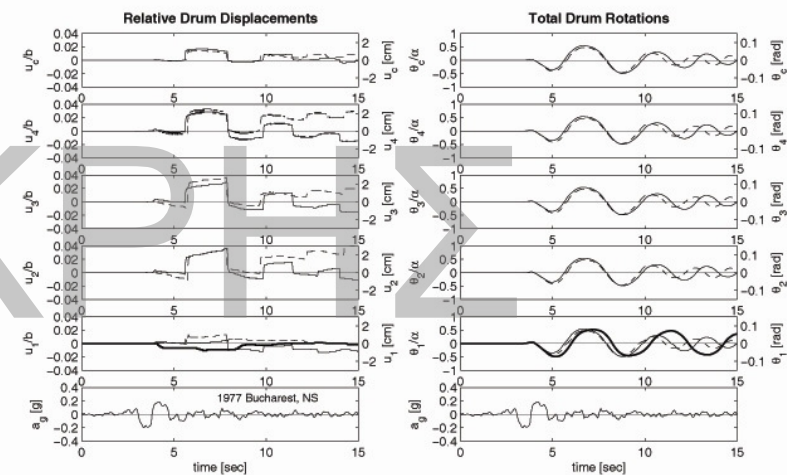
51



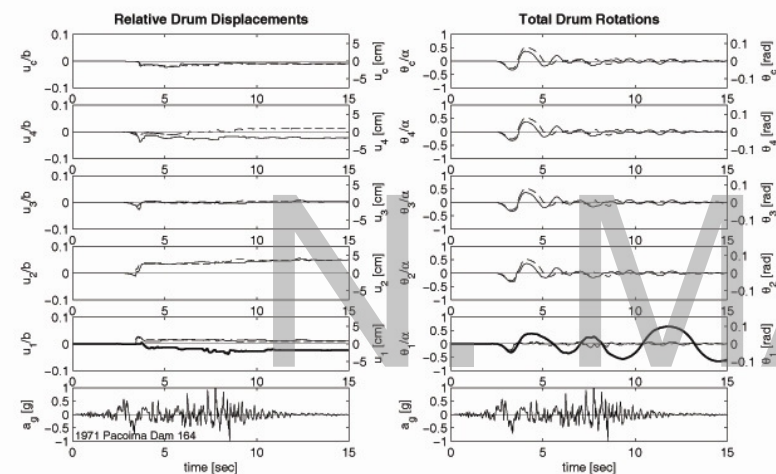
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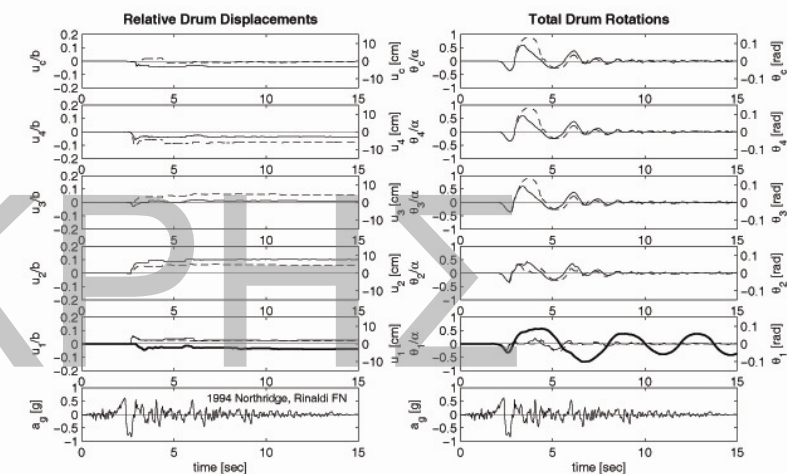
53



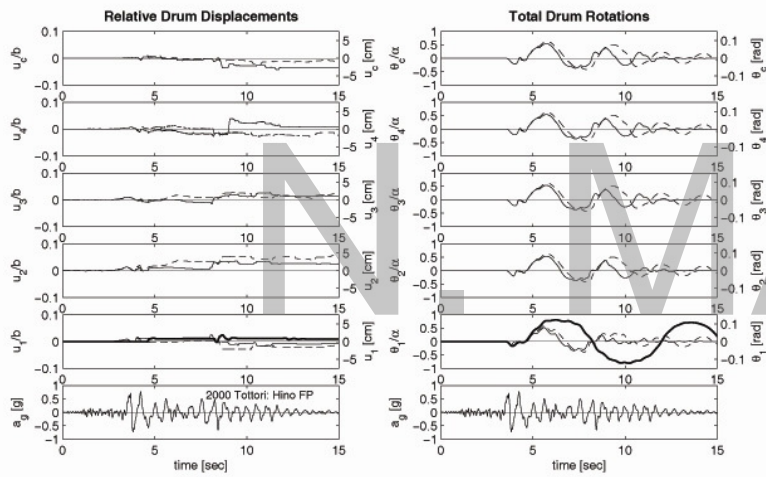
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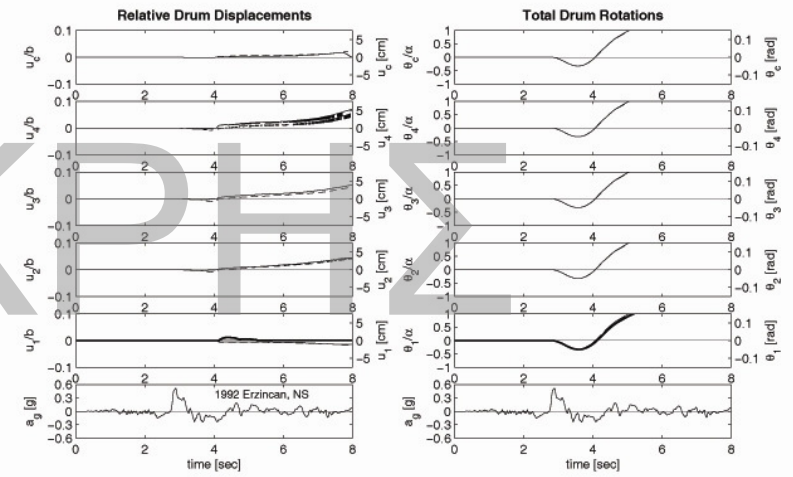
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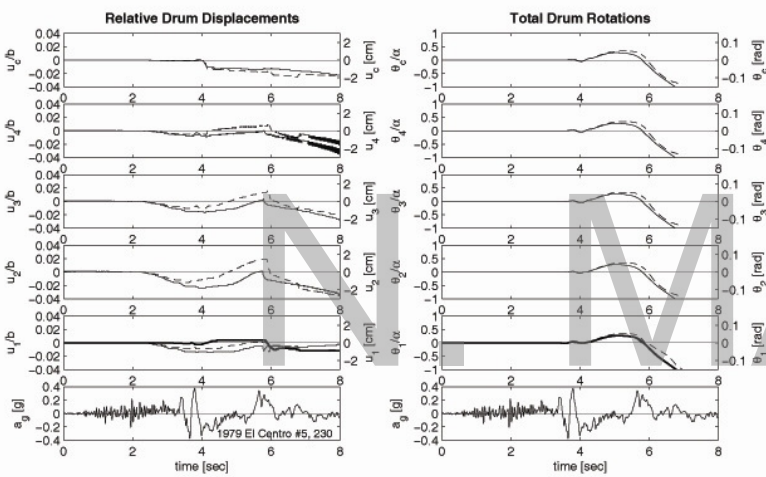
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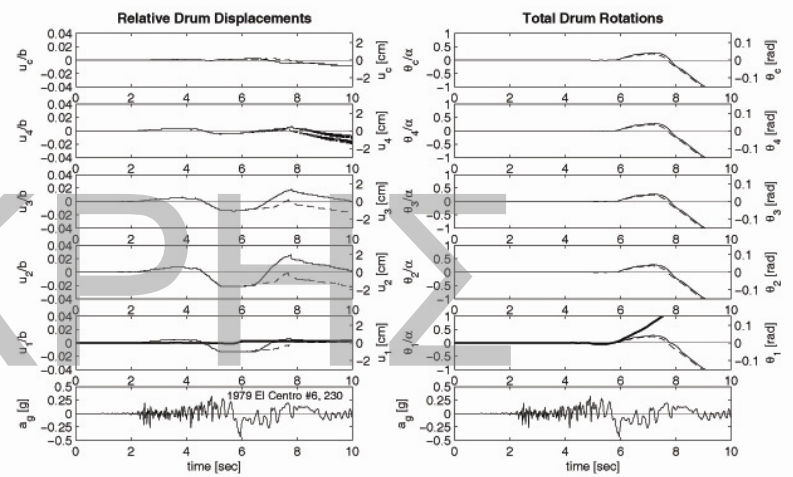
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58

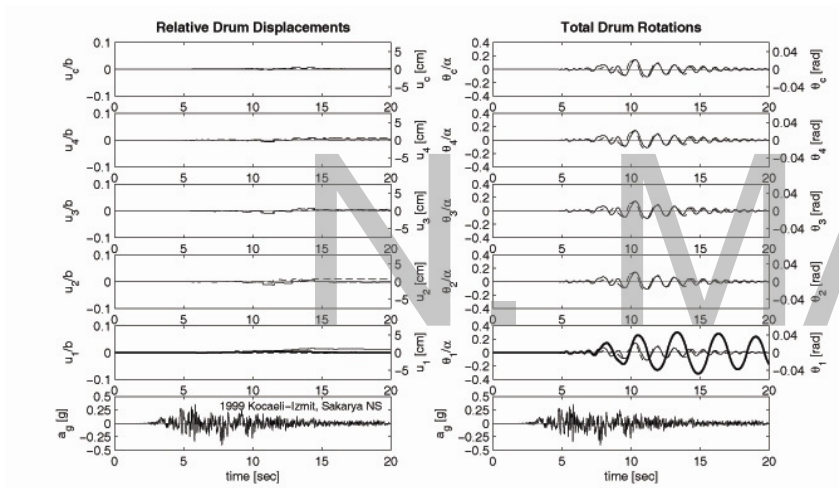


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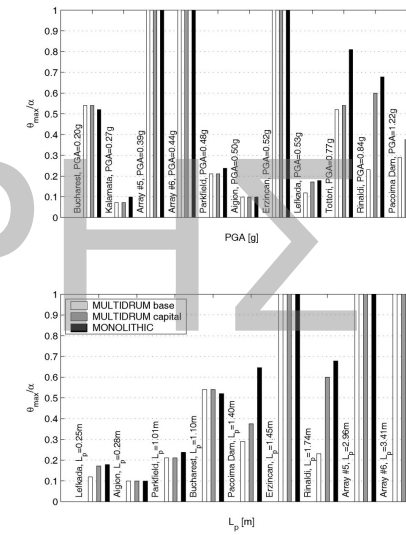


60

Peak column rotations from various historic strong earthquake motions



61



62

N. MAKΡΗΣ